Breath gas analysis for estimating physiological processes using anesthetic monitoring as a prototypic example

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Abstract—Analysis of exhaled trace gases is a novel methodology for gaining continuous and non-invasive information on the clinical state of an individual. This paper serves to explore some potential applications of breath gas analysis in anesthesia, describing a monitoring scheme for target site concentrations and cardiac output via physiological modeling and real-time breath profiles of the anesthetic agent. The rationale given here is mainly simulation-based, however, the underlying concepts are directly applicable to a routine clinical setting.

I. INTRODUCTION

Breath analysis is a relatively young field of research centering on the detection and quantification of volatile organic compounds (VOCs) appearing in human breath [1]. Such trace gases are either released endogenously or exogenously, entering the body as a result of exogenous exposure, eventually entering the bloodstream and being metabolized or excreted via exhalation, skin emission, urine, etc. Exhaled breath analysis employs some potential applications of breath gas analysis in anesthesia, accounting for the blood stream and being metabolized or excreted via the body as a result of exogenous exposure, eventually entering the blood stream and being metabolized or excreted via exhalation, skin emission, urine, etc. Exhaled breath analysis is employed for medical testing/diagnosis and monitoring, offering the advantage of being non-invasive. Breath samples can be extracted as often as desired and can be measured in real-time as well as with breath-by-breath resolution, e.g., by using proton-transfer-reaction mass spectrometry (PTR–MS) [2]. Breath analysis hence is an optimal choice for gaining continuous information on the physiological state of an individual, even under challenging conditions, e.g., during operations or at an intensive care unit. Within this context, the present paper serves to explore some potential applications of breath analysis in anesthesia. Due to the current lack of appropriate in vivo data, the rationale given here is mainly simulation-based, however, the underlying concepts are directly applicable to a routine clinical setting. A core task in anesthesia is to control anesthetic depth by administering adequate amounts of the anesthetic agent to the target (effect) sites in the central nervous system (CNS). While a well-defined relationship between target site concentrations (TSCs) and the associated anesthetic/amnestic response can be expected, assessments of the latter usually rest on derivational variables that can relatively easily be accessed by direct measurement. In inhalation anesthesia, a quantity of considerable interest is the minimum alveolar concentration (MAC), defined as the end-tidal concentration of the agent at which 50% of the patients fail to respond to surgical incision. However, the MAC value is essentially a steady state concept. Indeed, during transient states following a modification of the inspired gas concentration (e.g., induction) the end-tidal agent concentration is a poor indicator for the TSC. A more reliable estimation of anesthetic CNS levels would hence be highly desirable [3]. Similarly, for intravenous drugs the respective serum level often serves as a surrogate for the underlying TSC. As has been suggested by several authors, the former might also be estimated via breath measurements, thus obviating the time-intensive analysis of blood samples. For perspective, a good agreement between breath propofol content (determined, e.g., by PTR–MS at \( m/z = 179 \)) and serum levels has been reported [4].

A second hallmark of anesthesia is the need for continuous monitoring of vital respiratory and hemodynamic parameters. While ventilation is usually adjusted automatically by means of a breathing circuit (for ensuring stable normocapnic conditions), perfusion (i.e., cardiac output \( Q_c \)) is a rather intricate quantity to determine, particularly due to the inaccessibility of current stroke volumes. Reliable measurements of \( Q_c \) are imperative for combating many circulatory complications, however, most of the conventional methods for pursuing this goal are either highly invasive (dye or thermal dilution) or cumbersome (ultrasonic techniques, impedance cardiology). Alternatively, it is well-known that \( Q_c \) can also be reconstructed from the breath dynamics of exhaled inert gases (Fick principle), which is the approach that we shall adopt here. The inert gas employed will be the anesthetic agent itself, i.e., no additional instrumentation is involved. Specifically, our goal is to describe a novel on-line monitoring scheme for \( Q_c \) and the desired TSCs using physiological modeling and breath profiles of the anesthetic drug. Our account is strongly influenced by the earlier demonstration in [5], however, it differs from the latter by providing some model validation with clinical data and by using an estimation procedure fully exploiting the underlying model structure. The presentation in the sequel focuses on the prototypic volatile anesthetic sevoflurane, which is a convenient choice in terms of clinical relevance, measurability and availability of experimental data [6]. Particularly, this agent can be detected in PTR–MS at \( m/z = 181 \) [7], thus allowing for direct real-time measurements of the associated alveolar (end-tidal) concentrations. Sevoflurane is especially suitable for tracking hemodynamic/respiratory events due to the compound’s low blood:gas partition coefficient \( \lambda_{b:air} = 0.6 \) [8], implying a high sensitivity of the associated breath output with respect to blood and ventilatory flow.
**II. SIMULATION AND ESTIMATION**

A. **Physiological model**

The usual compartmental approach is adopted for capturing the tissue accumulation of sevoflurane during inhalation anesthesia. The systemic part of the model is similar to previously developed physiologically based descriptions of sevoflurane pharmacokinetics [3] and incorporates three well-mixed functional units: brain tissue (target site), a richly perfused tissue (RPT) compartment (liver, kidneys, muscle), lumping together tissue groups with comparable blood:tissue partition coefficient $\lambda_{b:rpt} \approx 0.24$ [8], as well as a buffer tissue (fat), acting as a reservoir for the lipophilic agent sevoflurane. All three compartments receive a constant share of $\dot{Q}_c$ and are separated into the intracellular space and the vascular blood, whereby a venous equilibrium holds at these interfaces. It is postulated that the major route of sevoflurane uptake and decrease is respiration, governed by the alveolar ventilation $\dot{V}_A$. In particular, metabolic clearance is assumed to be negligible [6]. The lung is modeled by one single homogenous alveolar unit characterized by an average ventilation-perfusion ratio close to one in normal healthy patients at rest. Since both venous admixture and physiological dead space are higher during general anesthesia than in the awake state, a constant shunt fraction $q_s = 0.1$ and an alveolar dead space fraction $v_{ad} = 0.1$ are incorporated into the model [9]. Pulmonary gas exchange is assumed to be perfusion-limited, i.e., an instantaneous equilibrium is established between the end-capillary concentrations $C_{vc}$ and alveolar levels $C_A$, viz., $C_{vc} = C_A \lambda_{b:air}$. The model structure is presented in Fig. 1. For a detailed nomenclature we refer to Table I.

![Diagram](image)

From the previous assumptions the mass balance equation for the alveolar compartment reads

$$\dot{V}_A \frac{dC_A}{dt} = (1 - v_{ad}) \dot{V}_A (C_I - C_A) + (1 - q_s) \dot{Q}_c (C_v - C_A \lambda_{b:air}),$$  

where $C_I$ denotes the inhaled sevoflurane concentration and $\dot{V}_A = V_A + \lambda_{b:air} \dot{V}_c$ is the effective alveolar volume taking into account the amount of sevoflurane dissolved in capillary blood. Similarly, for the brain, richly perfused and storage tissue compartment we find that

$$\dot{V}_{br} \frac{dC_{br}}{dt} = q_{br} \dot{Q}_c (C_a - \lambda_{b:br} C_{br}),$$

and

$$\dot{V}_{rpt} \frac{dC_{rpt}}{dt} = (1 - q_{br} - q_{st}) \dot{Q}_c (C_a - \lambda_{b:rpt} C_{rpt}),$$

and

$$\dot{V}_{st} \frac{dC_{st}}{dt} = q_{st} \dot{Q}_c (C_a - \lambda_{b:st} C_{st}),$$

respectively. Here, the associated concentrations in mixed venous and arterial blood are given by the weighted means

$$C_v := q_{br} \lambda_{b:br} C_{br} + (1 - q_{br} - q_{st}) \lambda_{b:rpt} C_{rpt} + q_{st} \lambda_{b:st} C_{st},$$

and

$$C_a := (1 - q_s) C_A \lambda_{b:air} + q_s C_v,$$

respectively. Moreover, the measured (end-tidal) sevoflurane concentration equals

$$C_{measured} = (1 - v_{ad}) C_A + v_{ad} C_I.$$  

The clinical adequacy of the above formulation was tested by comparing the resulting model predictions to an ensemble of in vivo concentration profiles published in [3]. By adopting the reference values in Table I and setting the initial concentration of each compartment to zero, the simulated model dynamics are in good agreement with the observed data, see Fig. 2.

![Graph](image)
Note that during anesthesia induction the end-tidal sevoflurane profile yields a poor representation of the underlying TSC dynamics. Specifically, while the former readily approaches the desired MAC of about 2%, jugular venous blood levels are still in a transitory phase.

### B. Anesthetic monitoring: a proof of concept

As has been pointed out in the introduction, the variables $C_1$ and $C_A$ can be viewed as known or measurable quantities within a routine setting, while $\tilde{Q}_c$ will be interpreted as an additional time-varying parameter $\theta$ that has to be estimated from the available breath sevoflurane data. Its time evolution will be modeled as a random walk. By employing zero-order hold sampling and introducing process as well as measurement noise, (1)–(7) can straightforwardly be transformed into a discrete time-varying stochastic system of the form

$$
\begin{align*}
    x_k &= G_{k-1}(\theta_{k-1}) x_{k-1} + f_{k-1} + w_{k-1} \\
    \theta_k &= \theta_{k-1} + \delta \theta_k \\
    y_k &= H_k x_k + d_k + v_k,
\end{align*}
$$

(8)

in the state variable $x := (C_A \ C_{br} \ C_{rpt} \ C_{st})^T$, with the scalar output being given by $y_k := C_{measured,k}$. Here, the postulated sampling interval is 5 s, roughly corresponding to the duration of one respiratory cycle during normal breathing at 12 tides/min. We assume that $\{w_k\}$, $\{\delta \theta_k\}$, and $\{v_k\}$ can be simulated as Gaussian, white, zero-mean noise sequences with known covariance matrices $Q_k$, $T_k$, and $R_k$, respectively. Additionally, we assign the Gaussian prior densities

$$
p(x_0) \sim \mathcal{N}(0, O), \quad p(\theta_0) \sim \mathcal{N}(\Theta_0^{est}, \text{var}(\Theta_0^{est})),
$$

(9)

encapsulating our information on the initial sevoflurane concentrations as well as on the initial cardiac output. Here, $O$ denotes the zero matrix of appropriate size.

Using the representation in (8) we may directly aim at the joint estimation of $x$ and $\theta$ from the observable profile of the breath sevoflurane concentration $y$ by virtue of Bayesian filtering methods as illustrated above. Due to the lack of appropriate in vivo data, a sequence of data points $x_k$ is simulated from the undisturbed system by employing predefined profiles for $\tilde{Q}_c$, $\tilde{V}_A$, and $C_1$ (cf. Fig. 3), setting $x_0 = 0$ (i.e., we assume that no sevoflurane is present in the body at the onset of anesthesia). Subsequently, noisy output data $y_k$ are created from (8) by applying additive Gaussian perturbations with fixed variance $R_k = (0.008)^2$.

Sequential state and parameter reconstruction from the stacked observations $Y_k := (y_k, \ldots, y_1)$ can be achieved by virtue of a marginalized particle filtering scheme as introduced in [10]. Briefly, the central object of interest within this framework is the conditional (posterior) probability $p(x_k|\Theta_k, Y_k)$, which embodies all accessible information on $x_k$ and the parameter sequence $\Theta_k := (\theta_1, \ldots, \theta_k)$ up to time $k$. For the purpose of computing this density, it is instructive to note that, conditional on $\Theta_k$, (8) represents a linear Gaussian system, i.e., we may decompose

$$
p(x_k, \Theta_k|Y_k) = p(x_k|\Theta_k, Y_k)p(\Theta_k|Y_k),
$$

(10)

where the first factor $p(x_k|\Theta_k, Y_k) \sim \mathcal{N}(\hat{x}^+_k(\Theta_k), P^+_k(\Theta_k))$ can be determined analytically by means of the standard Kalman filter formulae. As for the second factor, using Bayes’ Theorem and taking into account the specific structure of (8) one finds the recursion

$$
p(\Theta_k|Y_k) = \frac{p(y_k|\theta_k, Y_{k-1})}{p(y_k|Y_{k-1})} p(\theta_k|\Theta_{k-1}, Y_{k-1}) \times p(\Theta_{k-1}|Y_{k-1}).
$$

(11)

The goal of particle filtering is to approximate this density by drawing $m \gg 1$ random samples $\{\Theta_k^+, 1, \ldots, \Theta_k^+, m\}$ from it, producing a point mass representation of the form $p(\Theta_k|Y_k) \approx m^{-1} \sum_j \delta_{\Theta_k^+, j}(\Theta_k)$. Here, $\delta$ denotes the Dirac delta point measure. Plugging this expression into (10) one may directly compute estimators of the form

$$
E\{\phi(x_k, \Theta_k)|Y_k\} = \int \phi(x_k, \Theta_k)p(x_k, \Theta_k|Y_k) d\Theta_k dx_k \\
\quad \approx \frac{1}{m} \sum_{j=1}^m E\{\phi(x_k, \Theta_{k,j}^+)|\Theta_{k,j}^+, Y_k\}.
$$

In the specific situation above, by setting $\phi(x_k, \Theta_k) = x_k$ we arrive at the MMSE estimate

$$
E\{x_k|Y_k\} \approx \frac{1}{m} \sum_{j=1}^m \hat{x}^+_k(\Theta_{k,j}^+),
$$

(12)

and similarly for $\phi(x_k, \Theta_k) = \theta_k$. From (11), by adopting the standard sampling importance resampling scheme [11] the particle trajectories $\Theta_{k,j}$ can be updated as follows:

1. Invoke Kalman filtering to obtain the a priori state estimates $x_k^+(\theta_{k-1,j}^+)$ as well as $P_k^+(\theta_{k-1,j}^+)$ and propagate $\theta_{k-1,j}^+$ through the system dynamics (8) to arrive at a priori particles $\theta_{k,j}^-$.
2. Use $y_k$ to compute the likelihoods $p(y_k|\theta_{k,j}^-, Y_{k-1}) \sim \mathcal{N}(H_k \hat{x}^+_k(\theta_{k-1,j}^-) + d_k, H_k P_k^+(\theta_{k-1,j}^-) H_k^T + R_k)$.
3. Resample $\theta_{k,j}^-$ according to a multinomial distribution $\{(\theta_{k,1}^-, q_1), \ldots, (\theta_{k,m}^-, q_m)\}$ with the normalized likelihoods $d_j = p(y_k|\theta_{k,j}^-, Y_{k-1})/\sum_j p(y_k|\theta_{k,j}^-, Y_{k-1})$.

In a final step, the new a posteriori particles $\theta_{k,j}^+$ are used in the measurement update of the corresponding Kalman filter. Summarizing, marginalized particle filtering for joint state and parameter estimation in models of the form (8) essentially incorporates running a bank of $m$ separate Kalman filters in parallel (each one being associated with a single particle trajectory $\Theta_{k,j}$) and combining them like in (12).

The applicability of this filtering scheme within the anesthetic monitoring framework introduced above is demonstrated in Fig. 3. Here, the parameters of the prior density $p(\theta_0)$ in (9) were defined as $Q_0^{est} = 8$ l/min and $\text{var}(\Theta_0^{est}) = (3)^2$. Following common practice, the process noise covariance matrices $Q_k$ and $T_k$ were tuned to ensure a satisfactory performance of the algorithm. In particular we set $T_k = (0.3)^2$ as a tradeoff between short transition times (for tracking, e.g., a step change in perfusion) and estimation accuracy.
The state and parameter estimates calculated from (12) faithfully reproduce their simulated counterparts. In particular, incidences such as abrupt drops in cardiac output appear to be trackable within a delay time that is adequate for enabling intra-operative interventions.

III. CONCLUSIONS AND FUTURE WORK

While we believe that the present approach can potentially contribute to facilitating real-time assessments of the anesthetic state on the basis of exhaled breath measurements, several aspects have to be investigated more deeply before this method can become clinically relevant, e.g., as a part of automated anesthesia delivery systems. A primary building block is the availability of a reliable physiological model for the endogenous concentration profiles of the inhalational/intravenous agent under study. Consequently, additional experimental efforts, data gathering and modeling attempts (accounting for substance-specific confounding factors, e.g., the redistribution of regional blood flow or possible metabolism/sequestration patterns in the pulmonary tract as in the case of propofol) are required in order to extend the validity of simple models such as the one presented above over a sufficiently wide range of possible dynamics. Moreover, further insights into the quantitative links between anesthetic depth and TSCs need to be gained.

In this sense, the previous analysis should mainly be seen as a proof of concept, coupling the high-frequency information obtainable from breath gas analytical techniques with well-established tools from signal processing in order to achieve a continuous monitoring of physiological processes.

IV. ACKNOWLEDGMENTS

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<table>
<thead>
<tr>
<th>Parameter</th>
<th>Symbol</th>
<th>Nominal value [units]</th>
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<tbody>
<tr>
<td>Concentrations</td>
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<td>[mmol/l]</td>
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<td>Storage tissue (fat)</td>
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